



## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification <sup>5</sup> :

G02B 5/08

(11) International Publication Number:

WO 94/0939

A1

(43) International Publication Date:

28 April 1994 (28.04.94)

(21) International Application Number:

PCT/US93/09511

(74) Agents: STALLMAN, Michael, A. et al., Limbach, Linbach &amp; Sutton, 2001 Ferry Building, San Francisco, CA 94111 (US).

(22) International Filing Date:

5 October 1993 (05.10.93)

(30) Priority data:

07/959,699

13 October 1992 (13.10.92)

US

(81) Designated States: JP, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).

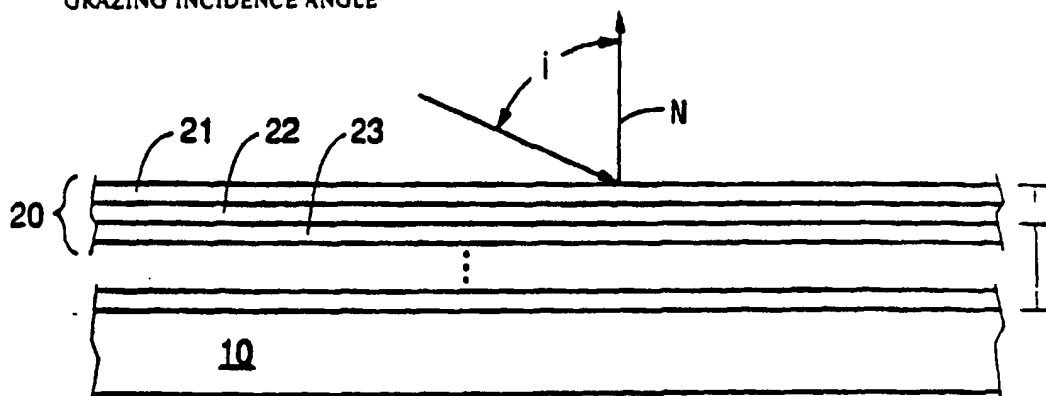
(71) Applicant: COHERENT, INC. (US/US); 5100 Patrick Henry Drive, P.O. Box 54980, Santa Clara, CA 95056-0980 (US).

Published

With international search report.

(72) Inventors: BAUMEISTER, Philip; 1588 Lilac Lane, Auburn, CA 95603 (US). FISCHER, Dennis; 14205 Edgehill Lane, Auburn, CA 95603 (US). TROST, David; 1201 California Street, San Francisco, CA 94109 (US).

(54) Title: OPTICAL COATING FOR REFLECTING VISIBLE AND LONGER WAVELENGTH RADIATION HAVING GRAZING INCIDENCE ANGLE



(57) Abstract

A coated reflector highly reflective of radiation having two different wavelengths over a wide range of incidence angles, including grazing incidence angles. The coated reflector can be employed in a waveguide for laser radiation useful for medical or other applications, such as a combined HeNe and CO<sub>2</sub> laser beam. Preferably, the coated reflector includes a metal substrate (10) and a multi-layer stack (20) thereon, the multi-layer stack (20) consists of alternating dielectric layers (21, 22, 23) of high and low refractive index material, each pair of adjacent high and low index layers of the stack (20) has a combined matched optical thickness substantially equal to an incident short (e.g., visible) wavelength multiplied by a factor  $M/2$ , and the total matched optical thickness of the stack (20) is substantially equal to  $(2N-1)\lambda_L/8$ , where  $M$  and  $N$  are positive integers and  $\lambda_L$  is an incident long wavelength (such as the wavelength of a CO<sub>2</sub> laser beam). Preferably, the substrate (10) is silver, the high index dielectric is zinc sulfide, and the low index dielectric is yttrium fluoride or cerium fluoride. In other embodiments, the invention is a hollow waveguide formed by folding a flat, coated substrate into a polygonal shape. Because the coated substrate is folded rather than rolled into a cylindrical tube, the bending stress on the coating is concentrated at the corners (32) of the polygonal waveguide rather than distributed over the waveguide's entire surface. Although the coating may crack at the corners (32) of the waveguide's polygonal cross section, the flat surfaces between the waveguide edges will be intact, and the cracks in the corners will have an insignificant effect on waveguide performance.

**FOR THE PURPOSES OF INFORMATION ONLY**

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	FR	France	MR	Mauritania
AU	Australia	GA	Gabon	MW	Malawi
BB	Barbados	GB	United Kingdom	NE	Niger
BE	Belgium	GN	Guinea	NL	Netherlands
BF	Burkina Faso	GR	Greece	NO	Norway
BG	Bulgaria	HU	Hungary	NZ	New Zealand
BJ	Benin	IE	Ireland	PL	Poland
BR	Brazil	IT	Italy	PT	Portugal
BY	Belarus	JP	Japan	RO	Romania
CA	Canada	KP	Democratic People's Republic of Korea	RU	Russian Federation
CF	Central African Republic	KR	Republic of Korea	SD	Sudan
CG	Congo	KZ	Kazakhstan	SE	Sweden
CH	Switzerland	LI	Liechtenstein	SI	Slovenia
CI	Côte d'Ivoire	LK	Sri Lanka	SK	Slovak Republic
CM	Cameroon	LU	Luxembourg	SN	Senegal
CN	China	LV	Latvia	TD	Chad
CS	Czechoslovakia	MC	Monaco	TO	Togo
CZ	Czech Republic	MG	Madagascar	UA	Ukraine
DE	Germany	ML	Mali	US	United States of America
DK	Denmark	MN	Mongolia	UZ	Uzbekistan
ES	Spain			VM	Vanuatu
FI	Finland				

-1-

OPTICAL COATING FOR REFLECTING VISIBLE AND LONGER  
WAVELENGTH RADIATION HAVING GRAZING INCIDENCE ANGLE

Field of the Invention

5       The invention relates to a coated optical reflector  
for reflecting radiation having two different  
wavelengths, such as visible and infrared radiation,  
and to a waveguide formed from such coated reflector.  
More particularly, the invention relates to a coated  
10       reflector that is highly reflective of radiation  
having two different wavelengths (such as combined  
HeNe and CO<sub>2</sub> laser radiation) incident over a range of  
incidence angles, including grazing incidence angles,  
and to a waveguide formed from such coated reflector.

15       Background of the Invention

Throughout this specification, including in the  
claims, the phrase "grazing incidence angle" is  
employed to denote an incidence angle in the range  
from 80 degrees to 90 degrees (where an incidence  
20       angle of zero degrees denotes normal incidence).

Waveguides and grazing incidence optics are  
employed in many commercial systems to reflect  
visible radiation (such as HeNe laser radiation), or  
infrared radiation (such as CO<sub>2</sub> laser radiation) and  
25       longer wavelength electromagnetic radiation, incident  
with a grazing incidence angle. When a purely  
metallic reflector is employed to reflect  
electromagnetic radiation at grazing incidence  
angles, the components of the radiation having S-  
30       polarization are reflected with high efficiency, but  
the components having P-polarization are reflected  
with low efficiency.

For example, Fig. 1 represents the reflectivity of  
gold (or silver) as a function of incidence angle, to

-2-

a beam of CO<sub>2</sub> laser (infrared) radiation. Fig. 1 shows that the reflectivity of gold (and silver) to the P-polarized component of the CO<sub>2</sub> laser beam decreases substantially with increasing incidence angle, but that the reflectivity to the S-polarized component of the CO<sub>2</sub> laser beam does not exhibit significant angular dependence. It will be appreciated by inspecting Fig. 1 that after a CO<sub>2</sub> laser beam undergoes multiple reflections (at grazing incidence) from a purely metallic waveguide, substantially the entire P-polarized component of the beam may be lost, undesirably causing a beam power loss of about 50% during propagation through the waveguide.

Figure 2 represents the reflectivity of silver as a function of incidence angle to visible radiation (orange light having wavelength 0.6 micrometers), and Figure 3 represents the reflectivity of gold as a function of incidence angle to the same visible radiation. Fig. 2 shows that the reflectivity of silver to the P-polarized component of the radiation decreases slightly with increasing incidence angle, but that silver's reflectivity to the S-polarized component of the radiation does not exhibit significant angular dependence. Fig. 3 shows that the reflectivity of gold to the P-polarized component of the 0.6 micrometer visible radiation depends strongly on incidence angle (although the minimum reflectivity occurs at a lower incidence angle than in Fig. 1), and that gold's reflectivity to the S-polarized component of the radiation increases with increasing incidence angle.

In an effort to address the problem of decreased reflectivity of metal (to visible radiation) in certain incidence angle ranges, it has been proposed to deposit stacks of alternating high and low

-3-

refractive index dielectric layers, each having a matched optical thickness of a quarter-wavelength, on metal to increase the metal's reflectivity to visible radiation. This technique efficiently increases reflectivity to normally incident visible radiation (having both P- and S-polarization), but it also increases reflectivity to visible radiation (of both polarizations) that is incident at grazing incidence angles (although with lower efficiency). However, if the difference between reflectivity to P-polarized and S-polarized radiation is large (for example, at a grazing incidence angle), an impractically large number of quarter-wave layers are required in a stack to achieve adequate reflectivity to both P-polarized and S-polarized components at grazing incidence angles.

Another limitation of the prior art technique described in the previous paragraph is that a stack of layers, each having quarter-wave thickness at a visible wavelength (such as a HeNe laser wavelength), will have no significant effect on infrared (or longer wavelength) radiation incident thereon. Thus, although a reflector coated with a multi-layer dielectric stack may have adequate reflectivity to visible radiation at grazing incidence, it will generally not have adequate reflectivity to infrared (or longer wavelength) radiation in the same grazing incidence angle range.

Waveguides and grazing incidence optics have been employed in commercial systems to reflect infrared radiation (such as CO<sub>2</sub> laser radiation) and longer wavelength radiation incident at grazing incidence angles. For example, U.S. Patent 4,805,987, issued February 21, 1989, and U.S. Patent 5,005,944, issued April 9, 1991, to Laakman, et al., disclose hollow lightpipes and lightpipe tip members that are highly

-4-

reflective of CO<sub>2</sub> laser radiation at grazing incidence angles. Each of these hollow members consists of a housing (said to consist preferably of flexible metal) and a highly reflective coating on the housing. The reflective coating is a dielectric material (such as silicon carbide) having refractive index with a real part less than one, and having sufficient thickness to assure bulk absorption properties.

However, conventional reflectors that are highly reflective of long wavelength electromagnetic radiation (including those described in U.S. Patents 4,805,987 and 5,005,944) over a range of incidence angles (including grazing incidence angles) have not also been highly reflective of substantially shorter wavelength radiation (e.g., visible radiation) over the same range of incidence angles.

Moreover, conventional reflectors of the type described in U.S. 4,805,987 and 5,005,944 are difficult to form into hollow waveguides (or lightpipes). This is because when flat substrates coated with commonly used reflective coatings of the type described in U.S. 4,805,987 and 5,005,944 are rolled to form tubes, stresses on the coatings often cause the coatings to crack (as explained at column 5, lines 50-60 of U.S. Patent 4,805,987). Use of reflective coating materials having high ductility (such as lead fluoride) may avoid the cracking problem, but such ductile materials are unsuitable for many applications because they are toxic.

It is also difficult to sputter (or otherwise deposit) a reflective coating (of the type described in U.S. 4,805,987 and 5,005,944) on a pre-formed hollow waveguide housing, particularly in the typical case that the hollow housing has very small diameter (e.g., one millimeter) and very long length (e.g.,

-5-

one meter). It is particularly difficult to deposit reflective coatings on such a hollow housing in a manner providing precise control of the thickness of the deposited layer.

5      Summary of the Invention

10      The invention is a coated reflector highly reflective of radiation having two different wavelengths over a wide range of incidence angles, including grazing incidence angles. One wavelength  
15      can be in the visible range and the other in the longer-than-visible range. The coated reflector can be employed in a waveguide for laser beams useful for medical and other applications (for example, combined HeNe and CO<sub>2</sub> laser beams). Preferably, the coated  
20      reflector includes a metal substrate, and a multi-layer stack on the substrate consisting of alternating dielectric layers of high and low refractive index material on the reflector, with each dielectric layer having optical thickness  
25      substantially equal to an incident short wavelength (such as the wavelength of a HeNe laser beam, or another visible wavelength), and with the total (matched) optical thickness of the multi-layer stack in the range from about .05 to about .225 of an  
30      incident long wavelength (such as the wavelength of a CO<sub>2</sub> laser beam, or another infrared or longer-than-visible wavelength). In variations on this preferred embodiment, each pair of adjacent high and low index layers of the multi-layer stack has a combined  
35      optical thickness substantially equal to the incident short wavelength multiplied by a factor  $M/2$ , where  $M$  is a positive integer (although the optical thickness of the high index layer need not equal that of the adjacent low index layer). More generally, the total optical thickness of the multi-layer stack is

-6-

preferably substantially equal to  $(2N - 1)\lambda_i/3$ , where  $N$  is a positive integer and  $\lambda_i$  is the incident long wavelength.

5 Preferably, the reflector is silver, the high refractive index dielectric material is zinc sulfide (or another high index dielectric that is substantially transparent to both visible and longer-than-visible radiation), and the low refractive index dielectric material is yttrium fluoride or cerium  
10 fluoride (or another low index dielectric that is substantially transparent to both visible and longer-than-visible radiation).

In a class of embodiments, the invention is a hollow waveguide having a polygonal cross-section,  
15 formed by folding a flat, coated substrate (typically a metal substrate coated with a multi-layer dielectric coating which may have low ductility). Because the coated substrate is folded into a polygonal waveguide, rather than rolled into a  
20 cylindrical tube, the bending stress on the optical coating is concentrated at the corners of the polygonal waveguide rather than distributed over the waveguide's entire surface. Although the coating may crack at the corners of the waveguide's polygonal  
25 cross-section, the flat surfaces between the waveguide edges will be intact. The cracks in the corners will have an insignificant effect on performance of the waveguide.

#### Brief Description of the Drawings

30 Figure 1 is a graph of the reflectivity of gold (and silver) to infrared electromagnetic radiation, versus incidence angle of the radiation.

Figure 2 is a graph of the reflectivity of silver to visible electromagnetic radiation, versus  
35 incidence angle of the radiation.



-7-

Figure 3 is a graph of the reflectivity of gold to visible electromagnetic radiation, versus incidence angle of the radiation.

5 Figure 4 is a side cross-sectional view of a preferred embodiment of the coated reflector of the invention.

10 Figure 5 is a graph of loss (one minus radiant reflectance) of silver coated with a dielectric layer of refractive index 1.8, versus optical thickness of the dielectric layer, for each of two grazing incidence angles (88 degrees and 89 degrees) of infrared electromagnetic radiation.

15 Figure 6 is a cross-sectional view of the coated reflector of Fig. 4, which has been folded into a hollow, polygonal waveguide.

Figure 7 is a perspective view of a second preferred embodiment of the coated reflector of the invention.

20 Figure 8 is a perspective view of the coated reflector of Fig. 7, which has been folded into a hollow, polygonal waveguide.

Figure 9 is a graph of the reflectance of a coated reflector, having a twelve-layer dielectric stack and embodying the invention, as a function of wavelength.

25 Figure 10 is a graph of the reflectance of a coated reflector, having a sixteen-layer dielectric stack and embodying the invention, as a function of wavelength.

30 Figure 11 is a graph of loss (one minus reflectivity) for a class of preferred embodiments of the invention, versus the number of periods (adjacent high and low dielectric layer pairs in the multi-layer dielectric stack thereof), in response to incident radiation having a 10.6 micrometer wavelength.

35

-8-

Detailed Description of the Preferred Embodiments

A preferred embodiment of the inventive reflector will be described with reference to Figure 4. As shown in Fig. 4, the reflector includes reflective substrate 10, and multi-layer dielectric stack 20 coated on substrate 10. Stack 20 includes dielectric layers (including layers 21, 22, and 23) having alternating high and low refractive indices (i.e., the refractive indices of layers 21 and 23 are substantially equal to a first one of a high value and a low value, and the refractive index of layer 22 is substantially equal to the other one of the high value and the low value). Preferably, each of the layers of stack 20 has an optical thickness (matched at the incidence angle of the radiation) substantially equal to a quarter-wavelength of visible electromagnetic radiation to be reflected by the coated reflector of Fig. 4. In alternative embodiments, each pair of adjacent high and low index layers of stack 20 has a combined optical thickness (matched at the incidence angle of the radiation) substantially equal to a half-wavelength (or multiple thereof) of the visible electromagnetic radiation to be reflected (although the optical thickness of the high index layer need not equal that of the adjacent low index layer).

Throughout the specification, including in the claims, the expression "optical thickness" of a layer denotes the "matched" optical thickness of the layer (unless specified otherwise to the contrary). The term "matched" is employed in the following sense.

Suppose that the  $i$ th layer of a multi-layer dielectric stack has a metric thickness  $t_i$  and a refractive index  $n_i$ . At normal incidence, the optical thickness OT of the layer is the product of  $t_i$  and  $n_i$ , namely  $OT = (n_i)(t_i)$ . At grazing incidence angles

-9-

(e.g., 88 degrees), the foregoing formula does not accurately express the layer's optical thickness, because optical thickness at grazing incidence is increased to compensate for the difference in path lengths of the refracted rays in the stack. The match optical thickness,  $OT|_{\text{matched}}$ , is approximately equal to  $(n_1)(t_1)/[1 - (n_0^2)/(n_1^2)]^{1/2}$ , where  $n_0$  is the refractive index of the incident medium (which is usually air with a refractive index of close to unity).

As an example, consider a layer of refractive index 2.22 that is to function at an incidence angle of 88 degrees. Its matched optical thickness,  $OT|_{\text{matched}}$ , is approximately equal to  $(n_1)(t_1)/[1 - (2.22)^{-2}]^{1/2} = 1.12(n_1)(t_1)$ .

A beam incident at each layer of multi-layer stack will undergo two reflections: a first portion of the beam will reflect from the top surface of the layer, and a second portion of the beam will reflect from the bottom surface of the layer. If the beam has normal incidence, the optical thickness of the layer is simply the product of the layer's physical thickness with its index of refraction. In the case that the beam has a grazing incidence angle, the optical thickness of the layer is approximately equal to  $(t)(n_1)[1 - (n_0/n_1)^2]^{-1/2}$ , where  $t$  is the layer's physical thickness,  $n_0$  has been defined above, and  $n_1$  is the refractive index of the layer itself.

Throughout the specification, including in the claims, the expression "optical thickness" of an entire multi-layer dielectric stack denotes the sum of the optical thicknesses of the individual layers of the stack.

In alternate embodiments of the invention, each layer of stack 20 has an optical thickness substantially equal to any odd integral multiple of a

-10-

quarter-wavelength (e.g.,  $3/4$  wavelength,  $5/4$  wavelength, and so on) of the visible electromagnetic radiation to be reflected thereby. In preferred embodiments, the total optical thickness of stack 20 is preferably in the range from about .05 to about .225 of an incident long (e.g., infrared) wavelength to be reflected thereby (for reasons to be explained below). In other preferred embodiments, the total optical thickness of the multi-layer stack is substantially equal to  $(2N - 1)\lambda_i/8$ , where N is a positive integer and  $\lambda_i$  is the incident long wavelength.

Substrate 10 is composed of (or coated with) material having high reflectivity to electromagnetic radiation having a first (longer-than-visible) wavelength and to electromagnetic radiation having a second (visible) wavelength. In a preferred embodiment, substrate 10 is made of silver (which is highly reflective of visible and infrared radiation having S-polarization, and of visible radiation having P-polarization, as explained with reference to Figs. 1, 2, and 3). However, silver may have inadequate durability for some applications. Accordingly, substrate 10 may consist of alternative materials, such as other metals (including pure aluminum or gold), or dielectric materials whose refractive index has a real part less than one. The substrate employed in the inventive reflector can be a metal foil or a metal extrusion.

It is also within the scope of the invention for substrate 10 to consist of a material that is not highly reflective (such as an extrudable alloy of aluminum) coated with a layer of highly reflective material (such as silver or pure aluminum or gold). The multi-layer dielectric stack of the invention is coated on such highly reflective layer. Throughout

-11-

the specification (including in the claims) the phrase "highly reflective" substrate and variations thereon denote not only substrates consisting entirely of highly reflective material, but also  
5 substrates coated with a highly reflective layer.

The reflector of Fig. 4 is designed reflect radiation having a wide range of incidence angles, "i," including grazing incidence angles in the range from 80 degrees to 90 degrees with respect to the  
10 normal axis, N. In accordance with the teaching of the previous paragraph, the Fig. 4 reflector will efficiently reflect visible radiation having a grazing incidence angle if stack 20 includes a sufficient number of quarter-wave layers, regardless  
15 of whether such radiation has S-polarization or P-polarization.

To ensure that the Fig. 4 reflector will also efficiently reflect longer-than-visible radiation having a grazing incidence angle, regardless of  
20 whether such radiation has S-polarization or P-polarization, the overall thickness, T, of multi-layer dielectric stack 20 is such that the optical thickness of stack 20 is approximately  $L/8$  (i.e., greater than or equal to  $.05L$ , and less than or equal  
25 to  $.225L$ , where  $L$  is a wavelength of the longer-than-visible wavelength to be reflected by the Fig. 4 reflector. The basis for this preferred optical thickness range can be appreciated by reference to Fig. 5. Fig. 5 shows "loss" (one minus reflectivity)  
30 of a silver substrate coated with a single dielectric layer of refractive index 1.8, versus optical thickness of the dielectric layer, for each of two grazing incidence angles (88 degrees and 89 degrees) of infrared radiation. The curves S1 and P1  
35 represent S-polarized and P-polarized components of such radiation, respectively, incident at an

-12-

incidence angle of 88 degrees, and the curves S2 and P2 represent S-polarized and P-polarized components of the radiation, respectively, incident at an incidence angle of 89 degrees. As shown in Fig. 5, in the case that the dielectric layer has zero thickness, the silver substrate has good reflectivity to the S-polarized components but poor reflectivity to the P-polarized components. In the case that the dielectric layer has quarter-wave optical thickness (corresponding to coordinate 0.25 along the horizontal axis), the coated silver substrate has good reflectivity to the P-polarized components but poor reflectivity to the S-polarized components. When the dielectric layer has optical thickness in the range from about 0.5L to .225L (where L is the wavelength of the incident infrared radiation), the coated silver substrate has good reflectivity to both the P-polarized and S-polarized components. The inventor has recognized that the loss of multi-layer dielectric stack 20 of Fig. 4 (to longer-than-visible radiation) has a dependence on overall optical thickness similar to that shown in Fig. 5, so that the overall thickness T of stack 20 is preferably such that stack 20's optical thickness is greater than or equal to .05L, and less than or equal to .225L, where L is a wavelength of the longer-than-visible wavelength to be reflected.

The dielectric layers comprising coating 20 should be transparent at both the visible and longer-than-visible wavelengths to be reflected. The high index layers can be zinc selenide or zinc sulfide, although the latter is generally preferable because it is transparent over broader range of visible wavelengths. The low index layers can be thorium fluoride, yttrium fluoride, and cerium fluoride, among others. Thorium fluoride is easy to deposit on

-13-

a substrate, and is relatively stress free in the thick layers usually necessary for infrared-reflective coatings. However, thorium fluoride may be unsuitable for some medical applications because it is somewhat toxic due to its slight radioactivity (and possibly also due to chemical toxicity).

Yttrium fluoride and cerium fluoride may cause difficulty with stress in the deposition process.

In a class of preferred embodiments, the Fig. 4 reflector is highly reflective of combined HeNe and CO<sub>2</sub> laser radiation, including visible HeNe laser radiation having wavelength of about 633 nm, and infrared CO<sub>2</sub> laser radiation having wavelength substantially equal to 10.6 micrometers, over a wide range of incidence angles, including grazing incidence angles. In some of these embodiments, substrate 10 is silver, the high index layers of stack 20 are zinc sulfide, and the low index layers of stack 20 are yttrium fluoride.

Of paramount importance is the selection of the number of layers of alternating refractive indices that are used in the inventive reflector. Although two different stacks may manifest a reflectance that is completely adequate at shorter wavelengths (for example, in the visible part of the spectrum), the reflectance in the longer wavelength spectral region may be entirely inadequate. As an example, Figures 9 and 10 are graphs of the reflectance of coated reflectors embodying the invention, having twelve-layer and sixteen-layer dielectric stacks, respectively, at a grazing incidence angle (in air) of 88 degrees as a function of wavelength.

The reflector of Fig. 9 is a silver substrate coated with twelve alternating layers of high refractive index material (zinc sulfide) and low refractive index material (lanthanum sulfide). Each

-14-

of the zinc sulfide and lanthanum sulfide layers has quarter-wave optical thickness at a control wavelength of 650 nm (matched at an 88 degree incidence angle).

5       The reflector of Fig. 10 is a silver substrate coated with sixteen alternating layers of high refractive index material (zinc sulfide) and low refractive index material (lanthanum sulfide). Each of the zinc sulfide and lanthanum sulfide layers has  
10       quarter-wave optical thickness at a control wavelength of 650 nm (matched at an 88 degree incidence angle).

15       Except for narrow dips in reflectance near 530 nm, the reflectance for "s" linearly polarized flux is greater than 0.999 (in both Fig. 9 and Fig. 10). The reflectance at 633 nm for "p" linearly polarized flux is adequate (in both Fig. 9 and Fig. 10).

20       However, Fig. 11 shows that at the much longer wavelength of 10.6 micrometers, the Fig. 9 embodiment has very different loss (one minus radiant reflectance) characteristics than does the Fig. 10 embodiment. Fig. 11 depicts the loss for a class of preferred embodiments of the invention, versus the number of periods (adjacent high and low dielectric layer pairs in a multi-layer dielectric stack), in  
25       response to incident radiation having a 10.6 micrometer wavelength. Each dielectric layer in each such preferred embodiment has quarter-wave optical thickness at a control wavelength of 650 nm, matched  
30       at an 88 degree incidence angle. In Fig. 11, the left bar for each period represents loss for radiation having "s" polarization (incident in air with an incidence angle of 88 degrees) and the right bar for each period represents loss for radiation  
35       having "p" polarization (incident in air with an incidence angle of 88 degrees).



-15-

The bars identified by reference character "A" in Fig. 11 represent the six-period embodiment of Fig. 9, and indicate that the loss is well below 0.005 for both "s"-polarized and "p"-polarized radiation.

5 However, the bars identified by reference character "B" in Fig. 11 represent the eight-period embodiment of Fig. 9, and indicate that the loss for this embodiment is substantially different for "s"-polarized and "p"-polarized radiation (the loss for  
10 "s"-polarized radiation is about 25%, which is unacceptably high for most applications).

When even more periods are used (e.g., for ten periods, as identified by reference character "C"), the loss for both linear polarizations is again  
15 acceptably low. However, for eighteen periods (as identified by reference character "D"), the loss is again substantially different for "s"-polarized and "p"-polarized radiation, and the loss for "p"-polarized radiation is unacceptably high for most  
20 applications.

The strong dependence of loss on the number of periods of a reflector coated with a multi-layer dielectric stack can be explained as follows. A reflector coated with a single dielectric layer has a  
25 loss which depends strongly on the dielectric layer's optical thickness (for a given wavelength  $\lambda$ , matched at a given angle). The loss is low (typically, acceptably low) for both "s" and "p" polarizations when the optical thickness is  $\lambda/8$ ,  $3\lambda/8$ , or  $5\lambda/8$ .  
30 However, the loss for "p" polarized flux is much higher than for "s" polarized flux (and typically, unacceptably high) when the optical thickness is an odd integral multiple of a quarter wavelength  $\lambda$  (i.e.,  $\lambda/4$ ,  $3\lambda/4$ ,  $5\lambda/4$ , and so on), and the loss for  
35 "s" polarized flux is much higher than for "p" polarized flux (and typically, unacceptably high)

-16-

when the optical thickness is equal to  $\lambda/2$  or a multiple of  $\lambda/2$ . Choice of an optical thickness of  $\lambda/8$ ,  $3\lambda/8$ , or  $5\lambda/8$  for the layer represents a compromise, in that although the loss is less for one or other of the polarizations at the quarterwave or halfwave optical thicknesses, the loss is still acceptably low at the "compromise" optical thicknesses.

The inventors have recognized that in preferred embodiments of the inventive coated reflector, the total optical thickness of the multi-layer stack is in the range from about .05 to about .225 of an incident long wavelength (because the multi-layer stack can be approximated as a single layer of a dielectric material whose index is the mean of the high and low index layers of the stack). More generally, the inventors have recognized that the total optical thickness of the multi-layer stack should be substantially equal to  $(2N - 1)\lambda_L/8$ , where N is a positive integer and  $\lambda_L$  is the incident long wavelength. It is an important aspect of the invention that the number of periods of the multi-layer dielectric stack (of the inventive coated reflector) are selected so that the loss at the incident long wavelength (which can be 10.6 micrometers) is acceptably low.

In variations on the above-described embodiments, the multi-layer stack (on the reflective substrate of the invention) consists of alternating dielectric layers of high and low refractive index material, where the optical thicknesses of the high index dielectric layers are different from the optical thicknesses of the low index dielectric layers. For example, consider embodiments of the invention having structure: (air)(xHyL)<sup>q</sup>(silver), which indicates that a multi-layer stack having "q" periods is deposited

-17-

on a silver substrate, with each period consisting of a high index layer H of optical thickness "x" and a low index layer L of optical thickness "y." Examples of such embodiments include those in which the ratio y/x is substantially equal to 3, those in which the ratio y/x is substantially equal to 2, as well as those in which the ratio y/x is substantially equal to 1. In general, each pair of adjacent high and low index layers of the multi-layer stack should have a combined optical thickness (matched at the incidence angle) substantially equal to a half-wavelength (or multiple thereof) of the visible electromagnetic radiation to be reflected.

In other variations, the inventive optical reflector includes a substrate that is highly reflective of electromagnetic radiation having a first wavelength (such as a longer-than-visible wavelength) and a multi-layer stack of dielectric layers on the substrate (where at least one of the layers has a refractive index different than at least one other one of the layers). Each of the dielectric layers has a combined matched optical thickness selected for enhancing overall reflectivity of the optical reflector to electromagnetic radiation having a second wavelength (where the first wavelength is longer than the second wavelength, and the second wavelength can be a visible wavelength), and the stack has an overall matched optical thickness for enhancing reflection of radiation having the first wavelength. Preferably, the overall matched optical thickness of the stack is not less than  $.05\lambda_1(2N - 1)$  and not greater than  $.225\lambda_1(2N - 1)$ , where N is a positive integer and  $\lambda_1$  is the first wavelength.

Another embodiment of the invention is a hollow waveguide having a polygonal cross-section, formed by folding a flat, coated substrate into substantially

-18-

flat portions. Typically, the coated substrate is a metal substrate coated with a multi-layer, dielectric coating having low ductility. In one class of embodiments of the folded waveguide, the coated substrate is metal which has been anodized so that its anodized surface portion comprises a "coating." For example, the coated substrate can be formed by anodizing an aluminum extrusion to produce a surface layer of aluminum oxide on the aluminum.

An example of the folded waveguide of the invention is the five-sided waveguide shown in Figure 6. The waveguide of Fig. 6 is formed by folding the coated reflector of Fig. 4 into five flat surface portions separated by four edges 32. The coated reflector's multi-layer stack 20 faces inward (i.e., faces the waveguide's central longitudinal axis 30). A beam of radiation will thus multiply-reflect with grazing incidence from stack 20 as it propagates along axis 30 (generally perpendicularly to the plane of Fig. 6), and during each such reflection, a portion of the beam will propagate through stack 20 and then reflect with grazing incidence from substrate 10.

Because the Fig. 6 waveguide is produced by folding a flat, coated substrate, rather than rolling such a coated substrate into a cylindrical tube, the bending stress on coating 20 is concentrated at corners 32 rather than distributed over the entire inner surface of the waveguide. Although coating 20 may crack at corners 32, the flat surfaces of coating 20 between corners 32 will be intact. Any cracks at corners 32 will have an insignificant effect on performance of the waveguide.

Figure 7 is a perspective view of a second preferred embodiment of the inventive coated reflector, and Figure 8 is a perspective view of the

-19-

coated reflector of Fig. 7 folded into a hollow, polygonal waveguide.

5 The reflector of Fig. 7 includes substrate 40 (preferably, a metal extrusion or metal foil), and optical coating 50 deposited on substrate 40. Coating 50 can be a multi-layer dielectric coating identical (or similar) to coating 20 of Fig. 4, or it can be some other coating having characteristics (refractive index, transmissivity, optical thickness, and the like) selected for reflecting selected radiation. For example, where substrate 40 is aluminum, coating 50 can be a layer of aluminum oxide formed by anodizing a portion of the aluminum.

10 Substrate 40 is formed with thin portions between bottom indentations 42 and top indentations 52, and relatively thick portions separated by the thin portions. Coating 50 is deposited on indentations 52, as well as on the remaining (flat) portions of the top surface of substrate 40 (or is formed by anodizing the indented substrate). Coating 50 includes flat coating portions 53, 54, 55, and 56.

15 To produce the hollow waveguide of Fig. 8, the coated reflector of Fig. 7 is folded about each of its three thin portions, until the reflector's left face 43 meets right face 44. As shown in Fig. 8, when indentations 52 have been so folded, each of folded indentations 52 surrounds a cylindrical region (which may be an empty void). Each such cylindrical region is separated from the main, rectangular central cavity defined by the four inward-facing flat coating portions 53, 54, 55, and 56. Although, stresses on coating 50 at indentations 52 (during folding of the Fig. 7 reflector) may cause coating 50 to crack at each of the three cylindrical regions 52 of Fig. 8, flat surfaces 53, 54, 55, and 56 of coating 50 between regions 52 will be intact. Any

-20-

cracks at regions 52 of Fig. 8 will have no effect (or no more than an insignificant effect) on reflection of grazing incident radiation from surfaces 53-56 of the Fig. 8 waveguide.

5 In practice, we have found that folded regions 52 in Fig. 8 will sometimes become filled with displaced metal and/or cracked coating material during the folding process (and will not define empty voids). However, even in such cases, flat surfaces 53, 54,  
10 55, and 56 of coating 50 between regions 52 will be intact.

As is also apparent from Fig. 8, the scalloped profile of the bottom face of the Fig. 7 reflector causes the waveguide of Fig. 8 to have a smooth,  
15 cylindrical outer surface.

Various modifications and alterations in the structure and method of the invention will be apparent to those skilled in the art without departing from the scope and spirit of this  
20 invention. Although the invention has been described in connection with specific preferred embodiments, it should be understood that the invention as claimed should not be unduly limited to such specific embodiments.

-21-

## WHAT IS CLAIMED IS:

1. An optical reflector, including:

a substrate highly reflective of electromagnetic radiation having a first wavelength and a second wavelength, wherein the first wavelength is shorter than the second wavelength; and

a multi-layer stack of alternating high and low refractive index dielectric layers on the substrate, wherein each pair of adjacent ones of the layers has a combined matched optical thickness substantially equal to the first wavelength multiplied by a factor  $M/2$ , where  $M$  is a positive integer, and wherein the stack has an overall matched optical thickness for enhancing reflection of radiation having the second wavelength.

2. The reflector of claim 1, wherein the first wavelength is a visible wavelength and the second wavelength is a longer-than-visible wavelength.

3. The reflector of claim 1, wherein the overall matched optical thickness of the stack is substantially equal to not less than .05 of the second wavelength, and not greater than .225 of said second wavelength.

4. The reflector of claim 1, wherein the overall matched optical thickness of the stack is not less than  $.05\lambda_2(2N-1)$  and not greater than  $.225\lambda_2(2N-1)$ , where  $N$  is a positive integer and  $\lambda_2$  is the second wavelength.

5. The reflector of claim 1, wherein each of the layers has a matched optical thickness substantially equal to one quarter of the first wavelength.

-22-

6. The reflector of claim 1, wherein the substrate is composed of silver.

7. The reflector of claim 1, wherein the first wavelength is a wavelength of a HeNe laser beam.

5        8. The reflector of claim 1, wherein the second wavelength is substantially equal to 10.6 micrometers.

10       9. The reflector of claim 1, wherein the high refractive index dielectric layers are substantially transparent at both the first wavelength and the second wavelength, and the low refractive index dielectric layers are substantially transparent at both the first wavelength and the second wavelength.

15       10. The reflector of claim 9, wherein the substrate is silver, the high refractive index dielectric layers are zinc sulfide, and the low refractive index dielectric layers are yttrium fluoride.

20       11. The reflector of claim 1, wherein the substrate has substantially parallel indentations defining relatively thin portions of said substrate, wherein each of the relatively thin portions separates two relatively thick portions of the substrate, and wherein the relatively thin portions are sufficiently thin to enable the substrate to be folded along said indentations.

25

12. The reflector of claim 11, wherein the substrate is a metal extrusion.

13. The reflector of claim 11, wherein the substrate has a left face and a right face, and



-23-

wherein the indentations are such that when the substrate has been folded along the indentations until the left face meets the right face, the folded substrate encloses a main volume, and each of the  
5 indentations defines a region separate from the main volume.

14. A coated optical reflector highly reflective of electromagnetic radiation having grazing incidence, including:

10 a substrate having a top face and a bottom face, and substantially parallel indentations in at least one of the top face and the bottom face, wherein the indentations define thin portions of the substrate, each of the thin portions separates two relatively  
15 thick portions of the substrate, and the thin portions are sufficiently thin to enable the substrate to be folded along said indentations; and an optical coating on the top face.

15. The reflector of claim 14, wherein the  
20 substrate has a left face and a right face, wherein the indentations include top indentations in the top face, and wherein the top indentations are shaped such that when the substrate has been folded along the indentations so that the left face meets the  
25 right face, the folded substrate encloses a main volume, and each of the top indentations defines a region separate from the main volume.

16. The reflector of claim 14, wherein the substrate is a metal extrusion.

30 17. The reflector of claim 14, wherein the substrate is metal, and the optical coating includes an anodized surface portion of the substrate.

-24-

18. The reflector of claim 14, wherein the metal is aluminum, and the anodized surface portion is aluminum oxide.

5 19. The reflector of claim 14, wherein the substrate is highly reflective of electromagnetic radiation having a first wavelength and a second wavelength, wherein the first wavelength is shorter than the second wavelength, and wherein the coating is substantially transparent at the second wavelength  
10 and has an overall matched optical thickness for enhancing reflection of radiation having said second wavelength.

15 20. The reflector of claim 19, wherein the first wavelength is a visible wavelength and the second wavelength is a longer-than-visible wavelength.

21. The reflector of claim 19, wherein the first wavelength is a wavelength of a HeNe laser beam, and the second wavelength is substantially equal to 10.6 micrometers.

20 22. The reflector of claim 19, wherein the coating is a multi-layer stack of alternating high and low refractive index dielectric layers, wherein each of the layers has a matched optical thickness  
25 substantially equal to one quarter of said first wavelength, and wherein the stack has an overall matched optical thickness substantially equal to not less than .05 of said second wavelength, and not greater than .225 of said second wavelength.

30 23. A hollow waveguide, through which radiation can propagate along a longitudinal axis, including:

-25-

a folded, coated substrate having a polygonal cross-section in a plane perpendicular to the longitudinal axis, wherein the folded, coated substrate encloses a volume extending along the longitudinal axis, and wherein the folded, coated substrate is highly reflective of electromagnetic radiation having grazing incidence.

24. The waveguide of claim 23, wherein the folded, coated substrate has been formed by folding a substantially flat coated substrate, said substantially flat coated substrate having a top face, a bottom face, and an optical coating on the top face, wherein the optical coating of the folded, coated substrate faces the volume.

25. The waveguide of claim 24, wherein the substantially flat coated substrate includes a metal base having said top surface, and a multi-layer dielectric coating on said top surface.

26. The waveguide of claim 25, wherein the substantially flat coated substrate has substantially parallel indentations in the top face, and wherein the indentations are profiled so that when the substantially flat coated substrate has been folded into said folded, coated substrate, each of the indentations encloses a region separate from the volume.

27. The waveguide of claim 25, wherein the metal base is a metal extrusion.

28. The waveguide of claim 23, wherein the folded, coated substrate has been formed by folding a substantially flat coated substrate, wherein the

-26-

substantially flat coated substrate includes a metal base, and wherein the optical coating includes an anodized surface portion of the metal base.

5        29. The waveguide of claim 23, wherein the folded, coated substrate is highly reflective of electromagnetic radiation having a first wavelength and a second wavelength, wherein the first wavelength is a visible wavelength and the second wavelength is a longer-than-visible wavelength.

10        30. A method of forming a hollow waveguide, through which radiation can propagate along a longitudinal axis, including the steps of:

15        (a) forming a coated substrate by depositing an optical coating on a substantially flat substrate having a left face and a right face; and

20        (b) forming a folded, coated substrate having a polygonal cross-section in a plane perpendicular to the longitudinal axis, by folding the coated substrate to cause the left face to meet the right face, so that the folded, coated substrate encloses a volume extending along the longitudinal axis, wherein the folded, coated substrate is highly reflective of electromagnetic radiation having grazing incidence.

25        31. The method of claim 30, wherein the substantially flat substrate is a metal substrate, and the optical coating is a multi-layer dielectric coating on the metal substrate.

30        32. The method of claim 30, wherein the substantially flat substrate has substantially parallel indentations defining relatively thin portions thereof, wherein each of the relatively thin portions separates two relatively thick portions of

-27-

the substantially flat substrate, and wherein step (b) includes the step of folding the substantially flat substrate along said indentations.

5 33. The method of claim 32, wherein the indentations are shaped so that performance of step (b) causes each of said indentations to define a region separate from the volume.

10 34. The method of claim 30, wherein the folded, coated substrate is highly reflective of electromagnetic radiation having a first wavelength and a second wavelength, wherein the first wavelength is shorter than the second wavelength.

15 35. The method of claim 34, wherein the first wavelength is a visible wavelength and the second wavelength is a longer-than-visible wavelength.

36. The method of claim 30, wherein the substantially flat substrate is a metal substrate, and the optical coating includes an anodized surface portion of the metal substrate.

20 37. An optical reflector, including:  
a substrate highly reflective of electromagnetic radiation having a first wavelength; and  
a multi-layer stack of dielectric layers on the substrate, wherein at least one of the layers has a  
25 refractive index different than has at least one other one of the layers, and wherein each of the layers has a combined matched optical thickness for enhancing overall reflectivity of the optical reflector to electromagnetic radiation having a  
30 second wavelength, where the first wavelength is longer than the second wavelength, and wherein the

-28-

stack has an overall matched optical thickness for enhancing reflection of radiation having the first wavelength.

5        38. The reflector of claim 37, wherein the overall matched optical thickness of the stack is not less than  $.05\lambda_1(2N - 1)$  and not greater than  $.225\lambda_1(2N - 1)$ , where N is a positive integer and  $\lambda_1$  is the first wavelength.

10       39. The reflector of claim 37, wherein the second wavelength is a visible wavelength and the first wavelength is a longer-than-visible wavelength.

- 1 / 5 -

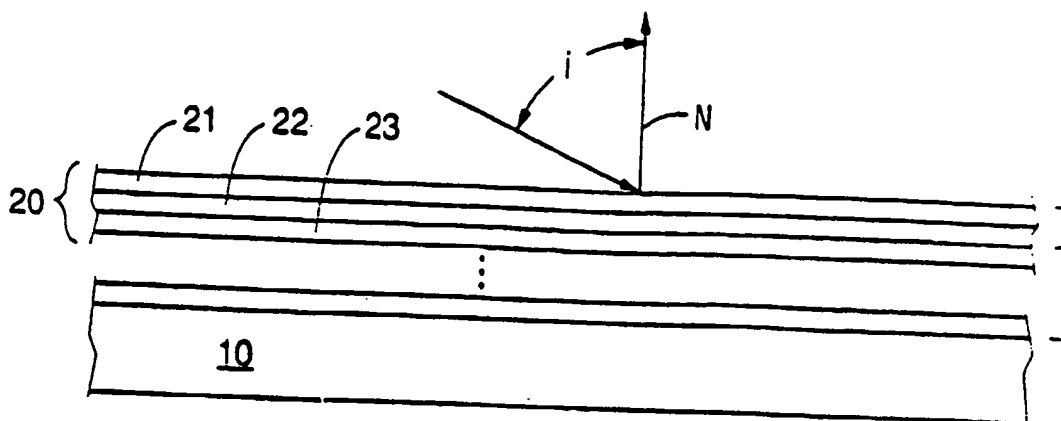


FIG. 4

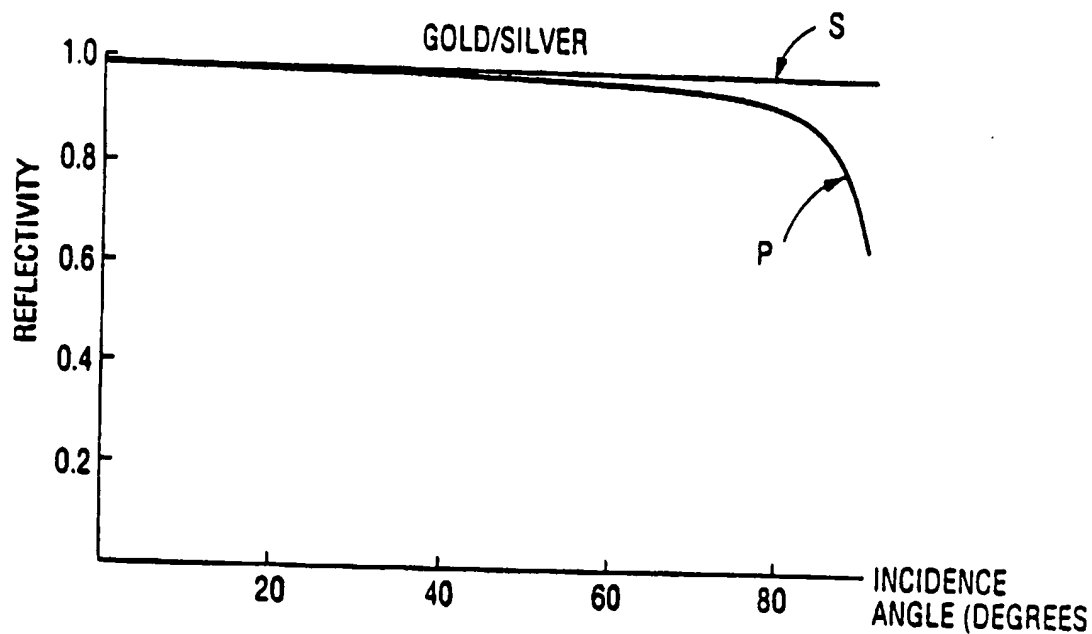


FIG. 1

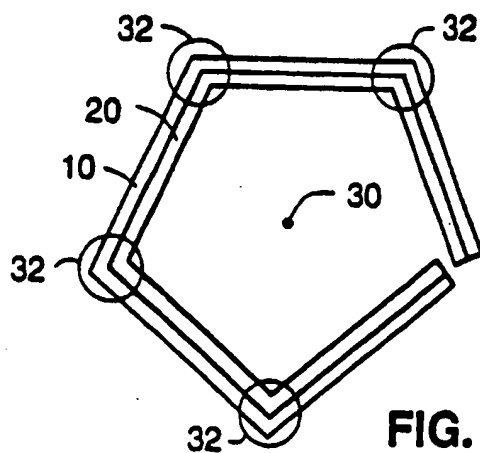


FIG. 6

- 2 / 6 -

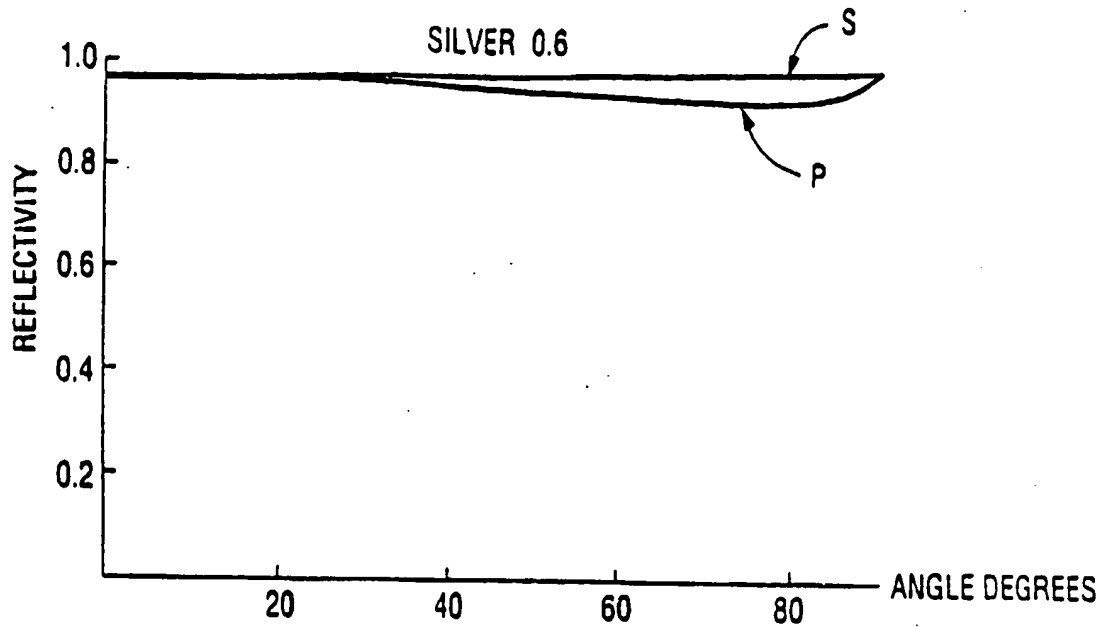


FIG. 2

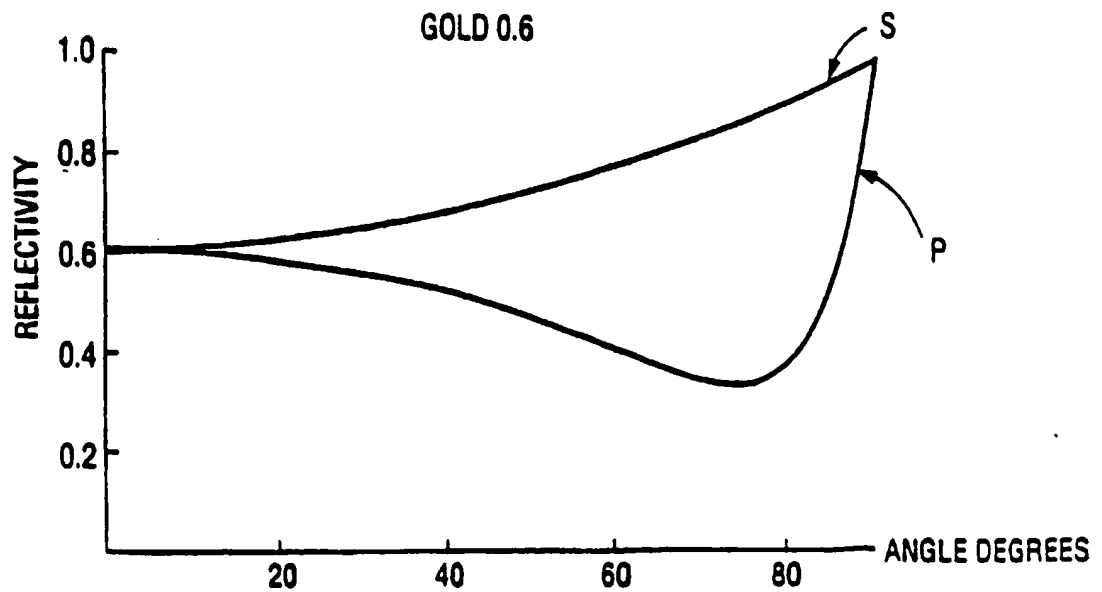


FIG. 3



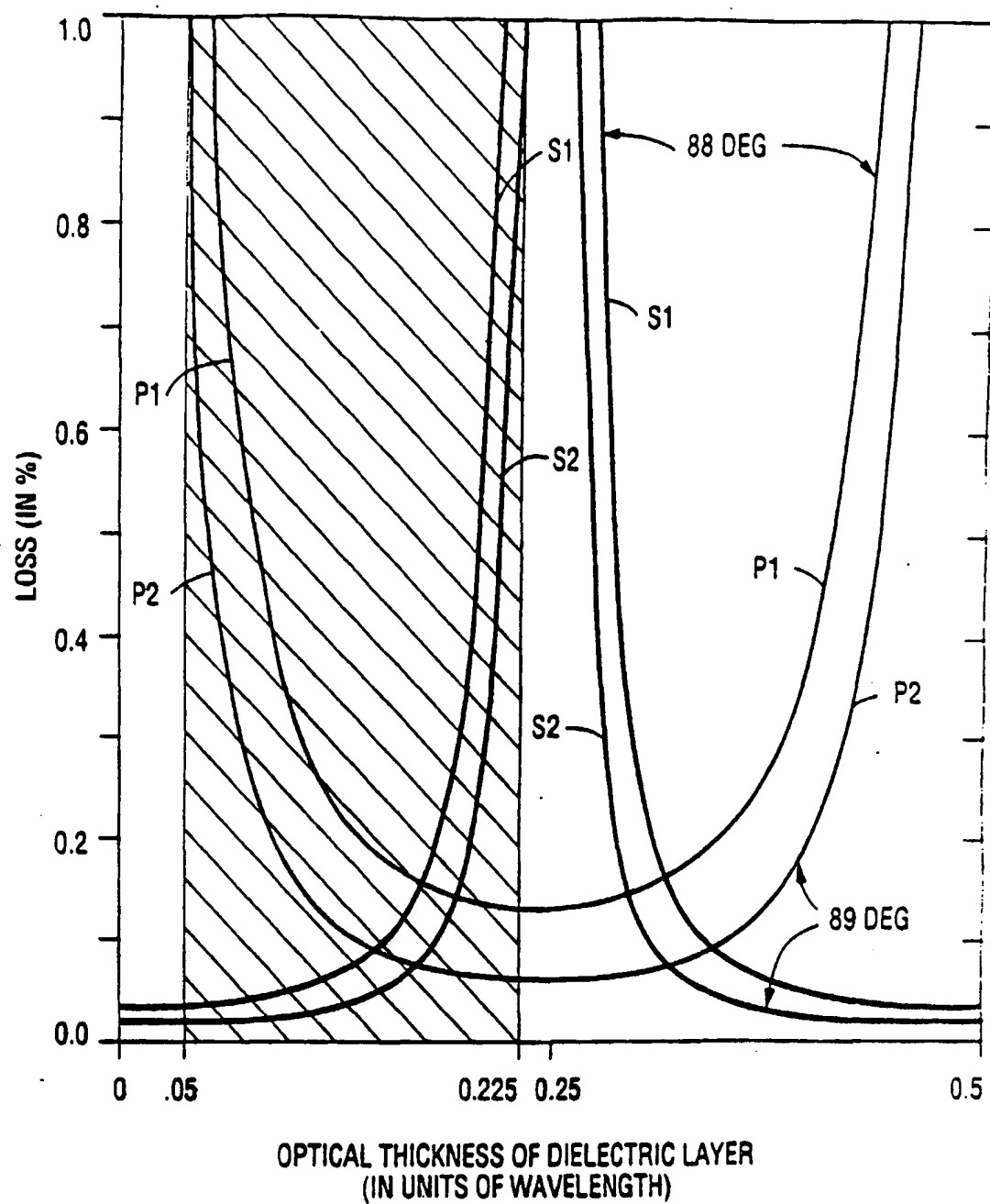
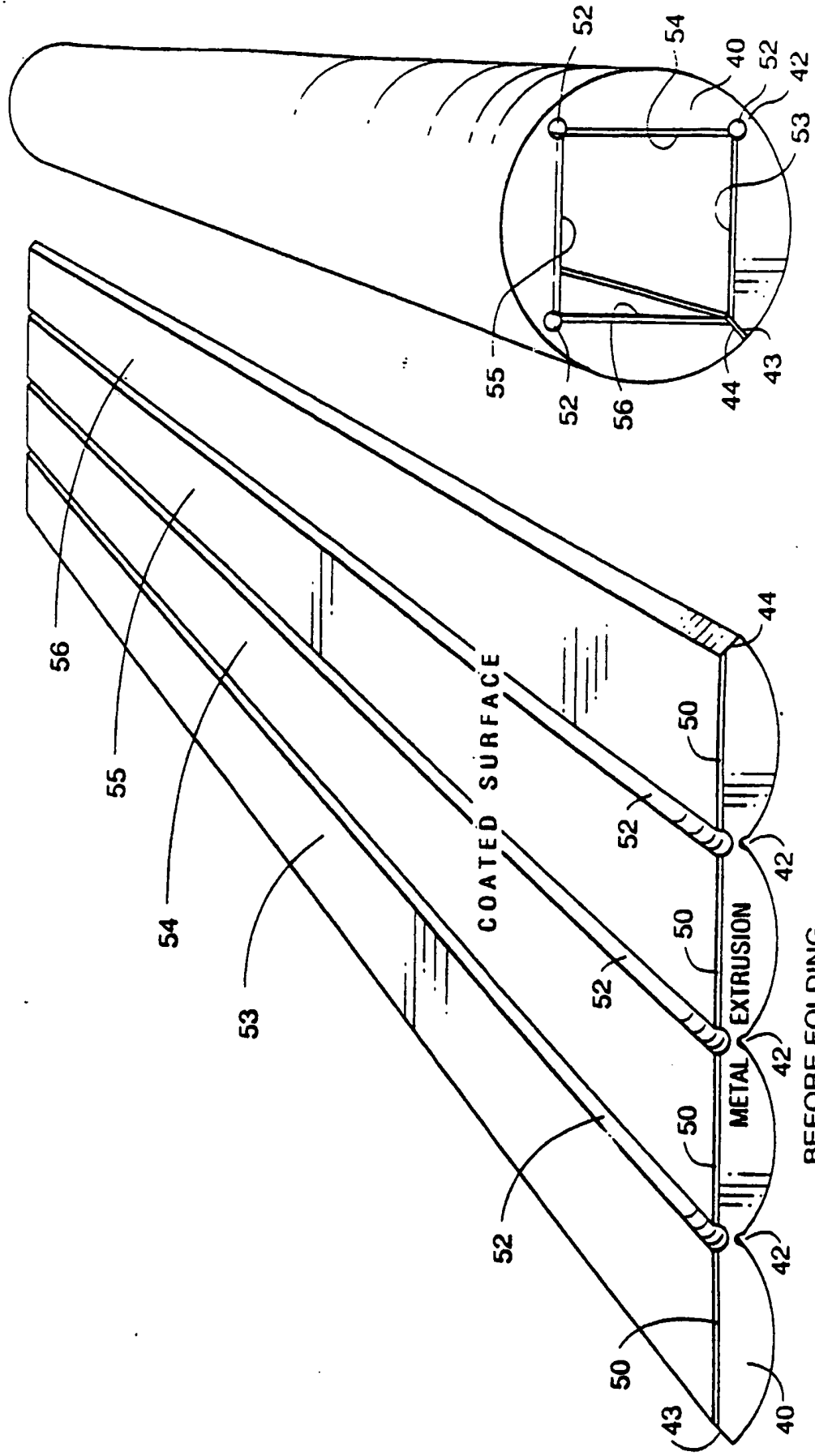
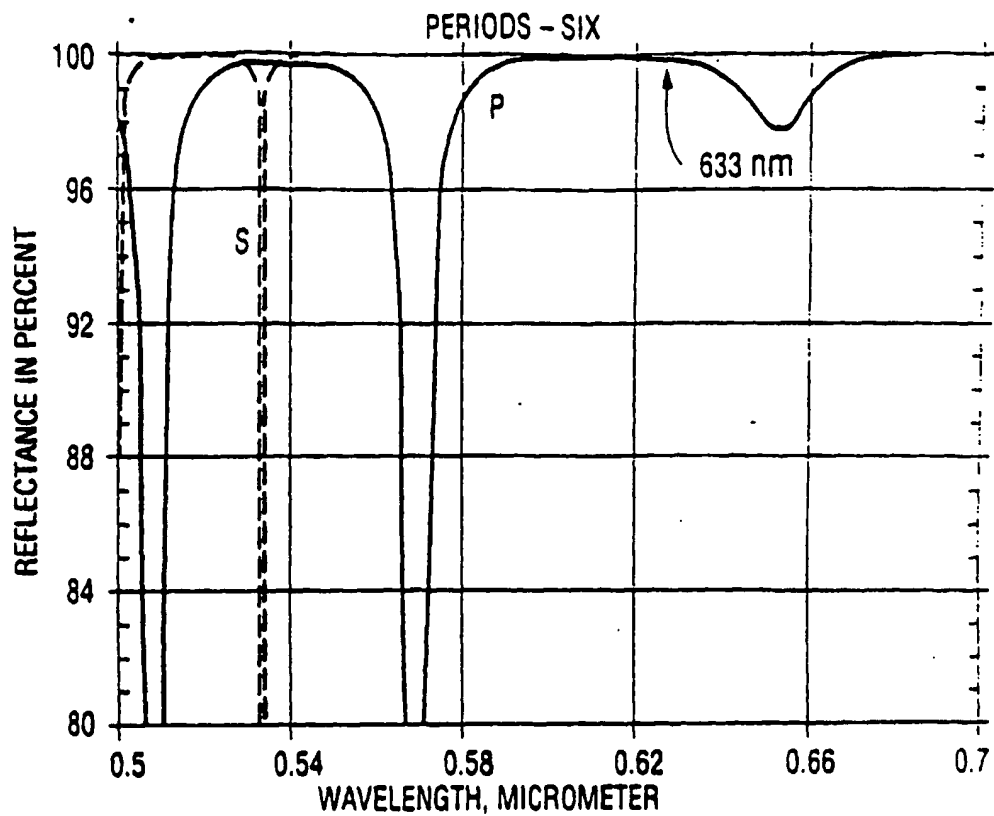
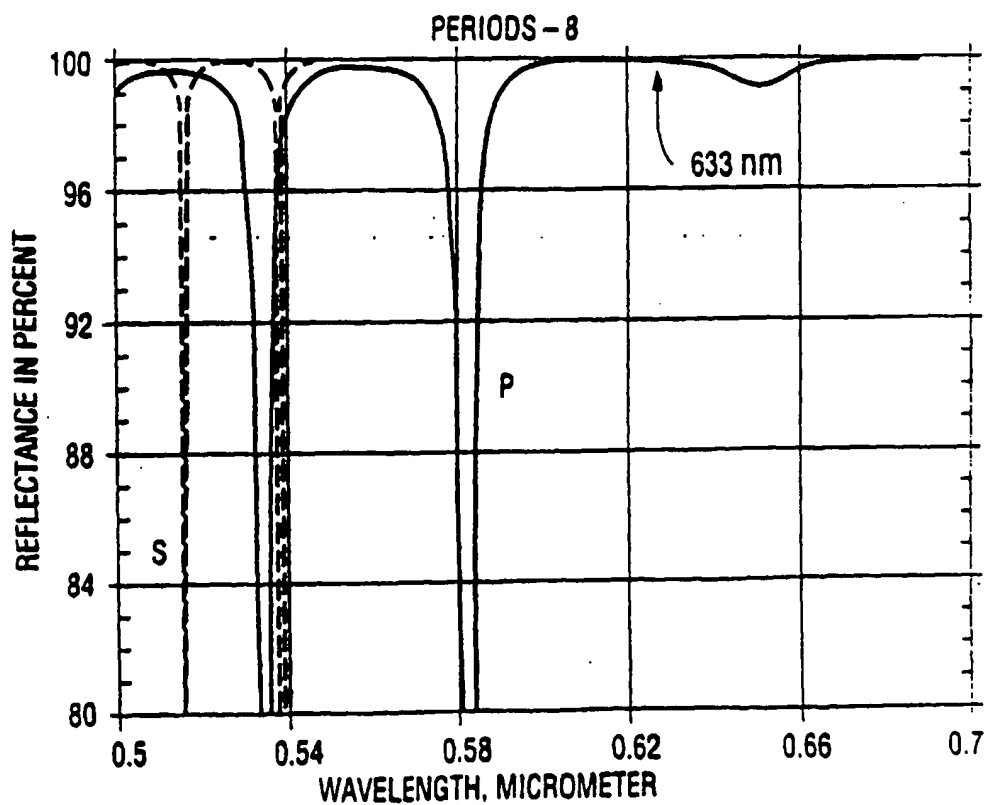


FIG. 5



**FIG. 8**  
AFTER FOLDING

**FIG. 7**  
BEFORE FOLDING

**FIG. 9****FIG. 10**

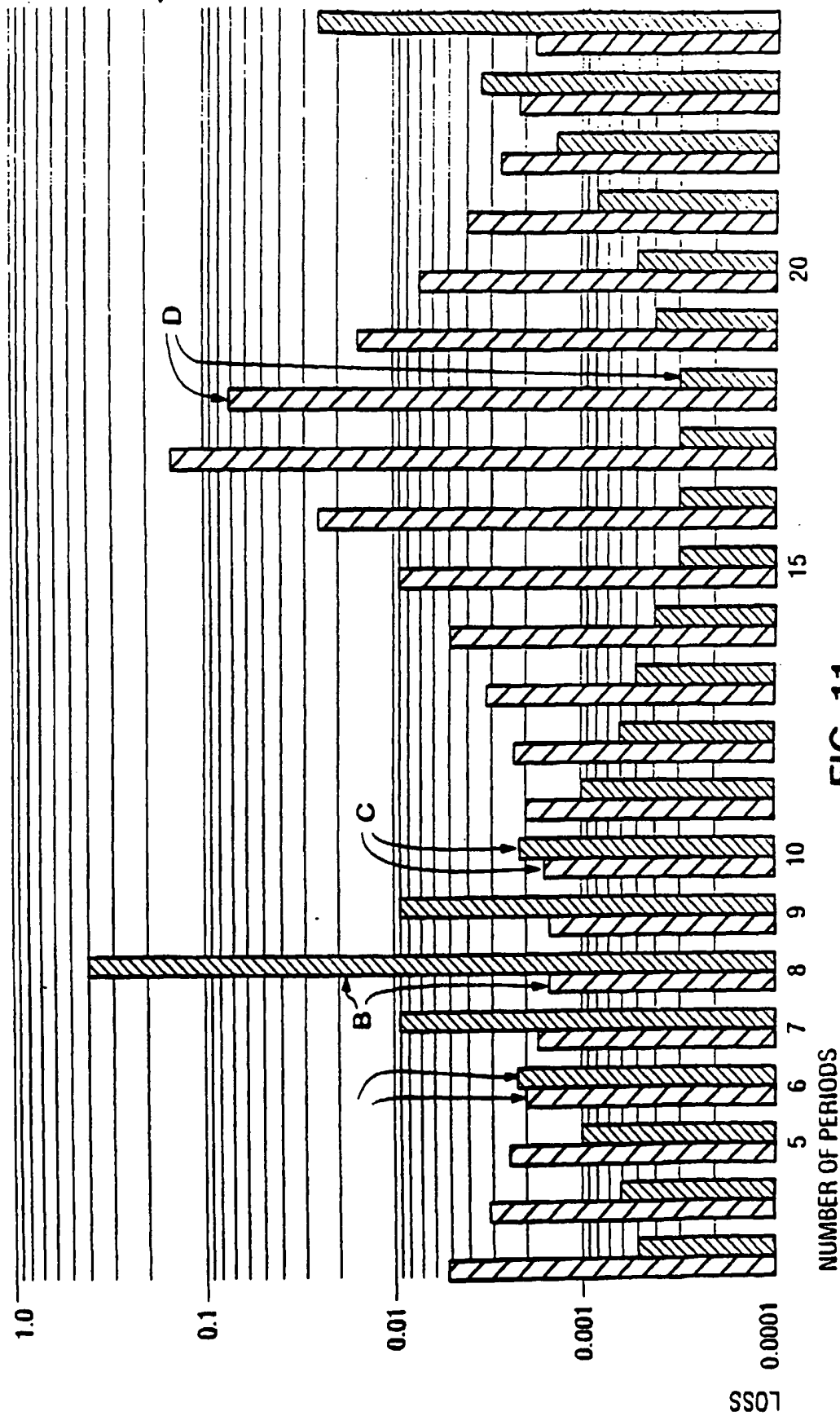


FIG. 11

<b>A. CLASSIFICATION OF SUBJECT MATTER</b> IPC 5 G02B5/08		
According to International Patent Classification (IPC) or to both national classification and IPC		
<b>B. FIELDS SEARCHED</b> Minimum documentation searched (classification system followed by classification symbols) IPC 5 G02B		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practical, search terms used)		
<b>C. DOCUMENTS CONSIDERED TO BE RELEVANT</b>		
Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	JOURNAL OF THE OPTICAL SOCIETY OF AMERICA - A vol. 2, no. 7, July 1985, NEW YORK US pages 1057 - 1065 J.B. SHELLAN 'DESIGN OF OPTIMUM HIGH-REFLECTIVITY COATINGS FOR GRAZING ANGLES OF INCIDENCE' see the whole document ---	1,6,14, 23,30, 31,37
A	WO,A,86 02775 (DURO-TEST) 9 May 1986 see page 18, line 20 - line 37 -----	1,2,20, 35,37,39
<input type="checkbox"/> Further documents are listed in the continuation of box C. <input checked="" type="checkbox"/> Patent family members are listed in annex.		
<b>* Special categories of cited documents:</b> "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document but published on or after the international filing date "I" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "A" document member of the same patent family		
Date of the actual completion of the international search 7 December 1993		Date of mailing of the international search report 05. 01. 94
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentaan 2 NL - 2280 LV Rijswijk Tel. (+ 31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+ 31-70) 340-3016		Authorized officer Malic, K

Form PCT-ISA, 218 (second sheet) (July 1992)

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
WO-A-8602775	09-05-86	AU-A- 3615884	15-05-86
		EP-A- 0197931	22-10-86
		JP-T- 62501109	30-04-87
-----			

**This Page is Inserted by IFW Indexing and Scanning  
Operations and is not part of the Official Record**

**BEST AVAILABLE IMAGES**

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- ☐ **BLACK BORDERS**
- ☐ **IMAGE CUT OFF AT TOP, BOTTOM OR SIDES**
- ☐ **FADED TEXT OR DRAWING**
- ☐ **BLURRED OR ILLEGIBLE TEXT OR DRAWING**
- ☐ **SKEWED/SLANTED IMAGES**
- ☐ **COLOR OR BLACK AND WHITE PHOTOGRAPHS**
- ☐ **GRAY SCALE DOCUMENTS**
- ☐ **LINES OR MARKS ON ORIGINAL DOCUMENT**
- ☐ **REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY**
- ☐ **OTHER:** \_\_\_\_\_

**IMAGES ARE BEST AVAILABLE COPY.**

**As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.**